

Mixed-state transport characteristics of magnesium diboride films

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We have investigated the low-temperature ($T < T_c/10$) mixed-state current-voltage (IV) response of magnesium diboride films beyond the point where the superconductivity is completely destroyed and the system enters the normal state. The resistance-versus-current $R(I)$ curves are extremely steep and featureless, with a critical current density j_c , marking the onset of dissipation, that is unusually high ($j_c > j_d/10$) with respect to the depairing current density j_d . At large flux densities $H_{c2}/10 \lesssim B \lesssim H_{c2}$, the $R(I)$ curve has a functional shape that is largely independent of B , indicating that the rise in resistivity with increasing current occurs mainly due to pair-breaking rather than flux motion. The macroscopic destruction current I^* , which drives the system normal, has a $[1 - \sqrt{B/H_{c2}}]$ flux-density dependence, suggesting that the vortices mainly reduce the effective cross section over which a current of effective density $j \sim j_d$ flows.

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INTRODUCTION AND BACKGROUND

When a superconducting state is formed, charge carriers correlate and condense into a coherent macroscopic quantum state. The formation of this state is governed principally by a competition between four energies: condensation, magnetic-field expulsion, thermal, and kinetic. The order parameter Δ , that describes the extent of condensation and the strength of the superconducting state, is reduced as the temperature T , magnetic field H , and electric current density j are increased. The boundary in the T - H - j phase space that separates the superconducting and normal states is where Δ vanishes, and the three parameters attain their critical values $T_c(H, j)$, $H_{c2}(T, j)$, and $j_d(T, H)$. j_d is the *depairing* or *pair-breaking* current density, which sets the intrinsic upper limiting scale for current transport in any superconductor.

In a transport measurement in finite flux density B , resistance appears above a threshold j_c at which flux vortices start to move. In a system with weak flux pinning, j_c is much lower than j_d and the response goes through alternate regimes of Ohmic (homogeneously linear dependence of V on I) and non-Ohmic behavior [1]. At very low driving forces (low j) there can be observable resistance due to thermally activated flux flow (TAFF) or flux creep. Then one encounters a non-linear response as current driven depinning sets in; in effect the number of mobile vortices is rising with j . This is incipient flux flow. At sufficiently larger j , the vortex motion is effectively free from the influence of pinning and the response becomes Ohmic again. We previously introduced the term free flux flow (FFF) for this linear regime [2]. Here the dissipation and resistivity should correspond to the canonical $\rho_f \sim \rho_n B/H_{c2}$ Bardeen-Stephen expression (sometimes large departures can occur for exceptional situations such as superclean systems and

narrow vortex cores where the internal energy-level spacing exceeds their widths). Beyond FFF, the response can become non-linear because of the heating of the electron gas [3] or changes in the electron distribution function [4]. Finally at yet higher currents, pair-breaking destroys superconductivity and drives the system normal and the resistance again becomes independent of current, being characteristic of the normal state. Our previous review article discusses some of these stages of dissipation. In $Y_1Ba_2Cu_3O_7$, the depinning critical current is sufficiently weak compared to the pair-breaking value that all of these regimes have been observed.

In MgB_2 the scenario has turned out to be completely different from the cuprates. The pinning in MgB_2 films is much stronger (because of its higher isotropy and ten times larger vortex cross section) and its T_c is intermediate in value (less than half that of $Y_1Ba_2Cu_3O_7$ or $Bi_2Sr_2CaCu_2O_8$). This boosts j_c while inhibiting thermally activated flux motion. On the other hand j_d has a much lower value than cuprates ($j_d(0) \sim 10^7$ A/cm² [5]). As a result j_c is within an order of magnitude of j_d and the IV curve remains dissipationless until $j_c \sim j_d$ and then quickly rises to the normal-state resistance more because of pair-breaking than flux motion.

Another distinction between MgB_2 and cuprates is its much lower normal-state resistivity ρ_n (lower than cuprates by 1–2 orders of magnitude). This leads to a much stiffer viscous coefficient η ($\approx \Phi_0 H_{c2}/\rho_n$) and consequently much lower vortex velocities for comparable values of applied j . Hence non-equilibrium effects related to changes in the macroscopic electronic distribution function [3, 4] are suppressed. All of these factors combine to produce an extremely steep non-linear IV curve influenced only secondarily by the motion of flux vortices, even when B approaches H_{c2} .

EXPERIMENTAL DETAILS

The samples are 400 nm thick films of MgB_2 fabricated using a two-step method whose details are described elsewhere [6, 7]. An amorphous boron film was deposited on a (1102) Al_2O_3 substrate at room temperature by pulsed-laser ablation. The boron film was then put into a Nb tube with high-purity Mg metal (99.9%) and the Nb tube was then sealed using an arc furnace in an argon atmosphere. Finally, the heat treatment was carried out at 900° C for 30 min. in an evacuated quartz ampoule sealed under high vacuum. X-ray diffraction indicates a highly c -axis-oriented crystal structure normal to the substrate surface with no impurity phases. The films were photolithographically patterned down to narrow bridges. In this paper we show data on three bridges, labelled S, M, and L (for small, medium, and large) with lateral dimensions 2.8×33 , 3.0×61 , and $9.7 \times 172 \mu\text{m}^2$ respectively. The lateral dimensions are uncertain by $\pm 0.7 \mu\text{m}$ and the thickness by ± 50 nm. Fig. 1(a) shows the sample geometry. The horizontal sections of the current leads contribute a small ($\sim 15\%$) series resistance to the resistance of the actual bridge when $B \gtrsim H_{c2}(T)$ and the entire material is normal. At low B in the mixed state, this extra contribution is frozen out because the current is spread out in these wider lead areas and hence its density is too low to cause dissipation. Then j is high only within the bridge itself and the leads do not contribute to the measured resistance.

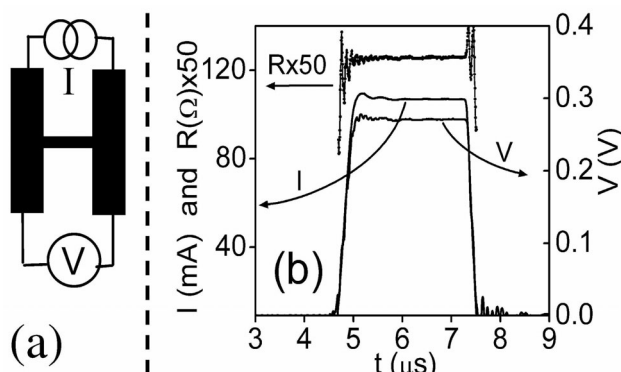


FIG. 1: (a) Sample geometry used for resistance measurement. At low values of j the wide lead areas add a constant resistance of about 15% of the total value. At high j this contribution is frozen out. (b) Pulse waveforms under worst-case conditions ($j = 9.7 \text{ MA/cm}^2$, $E = 83 \text{ V/cm}$, and $p = jE = 803 \text{ MW/cm}^3$ on the plateaus). The resistance rises to (90% of) its final value in about 50 ns from the (10%) onset of I .

The non-linear electrical transport measurements were made using a pulsed signal source with pulse durations ranging from 0.1 to $4 \mu\text{s}$ and a duty cycle of about 1 ppm. A conventional continuous DC method was employed for the very low currents ($I = 1.4 \mu\text{A}$). Fig. 1(b) shows pulse waveforms under the especially severe conditions of $j = 9.7 \text{ MA/cm}^2$, $E = 83 \text{ V/cm}$, and $p = jE = 803 \text{ MW/cm}^3$. The resistance rises to 90% of its final value in about 50 ns from the 10% onset of I . From a knowledge of the thermal conductivities and specific heat capacities of the film and substrate materials, and their mutual thermal boundary resistance, one can

calculate the total thermal resistance R_{th} for any pulse duration [1, 8]. Also if $R(T)$ has enough variation, the film's own resistance can be used as a thermometer to measure R_{th} . For films of $\text{Y}_1\text{Ba}_2\text{Cu}_3\text{O}_7$ (YBCO) on LaAlO_3 , which were used for most of our previous work, we found $R_{th} \sim 1\text{--}10 \text{ nK}\cdot\text{cm}^3/\text{W}$ at microsecond timescales [1, 3, 9]. In the case of our MgB_2 films, we expect R_{th} to be smaller because of sapphire's very high conductivity. However the five parameters required to calculate R_{th} from first principles are not all known for this film-substrate combination and MgB_2 has a very flat $R(T)$ below 50 K, so one can't measure R_{th} as was done for YBCO. We can, however, obtain an upper bound on R_{th} in the following way: Fig. 2 shows IV curves for sample L in zero field (This is the largest sample with the lowest surface-to-volume ratio, so that it represents the worst case thermal scenario.). The curves were measured with the sample in different thermal environments. Above some threshold current $I_d \sim 650 \text{ mA}$, the system abruptly switches into the normal state. The value of I_d is not sensitive to the thermal environment contacting the exposed surface of the film, confirming that the highly conductive sapphire, together with the greatly reduced heat input during the short pulse, prevents the film's temperature from rising significantly (It has been shown by Stoll et al. [10] that if there is sample heating, the thermal environment makes a significant difference because it will provide an additional path for the heat to flow through.). We show elsewhere [5] that this jump to the normal state occurs due to pairbreaking by the current [11]. At the point the system is driven normal, the power density reaches $p = jE = 1.01 \text{ GW/cm}^3$. This sets a gross upperbound of $R_{th} \sim 7 \text{ nK}\cdot\text{cm}^3/\text{W}$. Note that the main bottleneck of heat conduction is the film-substrate boundary resistance which is not strongly temperature dependent [8]. In the present work, typical p values are two orders of magnitude lower than the critical 1 GW/cm^3 and so we expect the temperature rise to be a small fraction ($\sim 1\%$) of T_c . A value of $j_d(0) \approx 2 \times 10^7 \text{ A/cm}$ was obtained from such zero-field IV curves [5]. The corresponding values for the zero-field pair-breaking currents are 240 mA, 257 mA, and 700 mA for samples S, M, and L respectively [5].

The magnetic field is applied normal to the film (parallel to the c axis) and the self field of the current is much lower than the applied fields used in this work. Further details of the measurement techniques have been published in a previous review article [1] and other recent papers [3, 9].

RESULTS AND ANALYSIS

Fig. 3(a) shows the $R(I)$ curves for sample M at different values of B in the $H_{c2}/10 \lesssim B \lesssim H_{c2}$ range. After the onset of dissipation, the resistance quickly rises to the full normal-state value. It should be noted that the plateaus do not correspond to FFF but to the normal state. Accordingly the resistance value changes very little with the applied B (the slight shift in plateau resistance at the highest flux densities can be understood in terms of spreading of resistance outside the bridge area into the current-lead areas as explained in the experimental section; fields approaching H_{c2} start driv-

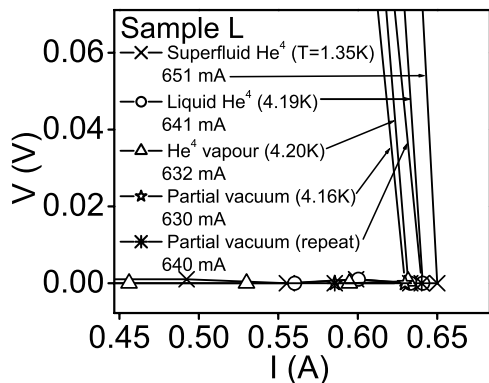


FIG. 2: IV curves in zero field for sample L in different thermal environments. The resistance is driven to its normal-state value (top parts of curves lie outside the panel) by currents of pair-breaking magnitudes. The absence of a significant systematic dependence on the thermal environment shows the paucity of sample heating.

ing the whole film normal so that the resistance of the wider current-lead areas is not frozen out). It is interesting to note that the overall shapes of the curves are almost independent of B . The curves of panel (a) can be made to overlap, as shown in Fig. 3(b), by merely shifting them vertically and horizontally by constant amounts. For a dissipation curve influenced by flux motion, one expects the function to depend on B . The vertical shift is not crucial as explained above. The horizontal shift corresponds to subtracting an amount I^* from I . I^* , which we call the destruction current, is the elbow point (arrow in Fig. 3(b)) below which R starts to fall below its normal-state value. In panel (c), this I^* is plotted versus the function $[1 - \sqrt{B/H_{c2}}]$, the meaning of which is explained below. It is seen that most of the data obey a roughly linear dependence that extrapolates back to the origin, consistent with the pinch-off model. Also we note that at the current scale of this phenomenon $I^* \sim 50$ mA is of the order of the pair-breaking current (257 mA) for this sample (For $B < 2$ T, the sample resistance becomes lower than the source impedance of the pulsed voltage source. As a result the relevant portion of the $R(I)$ curve is inaccessible. This external circuit issue is discussed elsewhere [5].).

We tentatively propose the following explanation for the $R(I)$ curve and its parallel shifts with B : Clearly the current scale for the curves is of the order of the pair-breaking current (please earlier discussion and reference [5]). This implies that pinning is so strong that vortex motion doesn't lead to enough dissipation to greatly contribute to $R(I)$. Then the perfect conductivity is destroyed mainly by pair-breaking and the field merely serves to suppress the effective j_d . We could not find in the literature any discussion of the field dependence of j_d . For the field range in question we propose that the main effect of increasing B is to "pinch off" the cross section by adding more vortices. At high $B \sim H_{c2}$, there will be some additional corrections as the field approaches its critical value, but for lower fields let's assume that the local j_d is unaffected by B , but only the macroscopic average j_d is reduced because of loss of cross-sectional area. In this case the destruction current I^* will equal j_d times the avail-

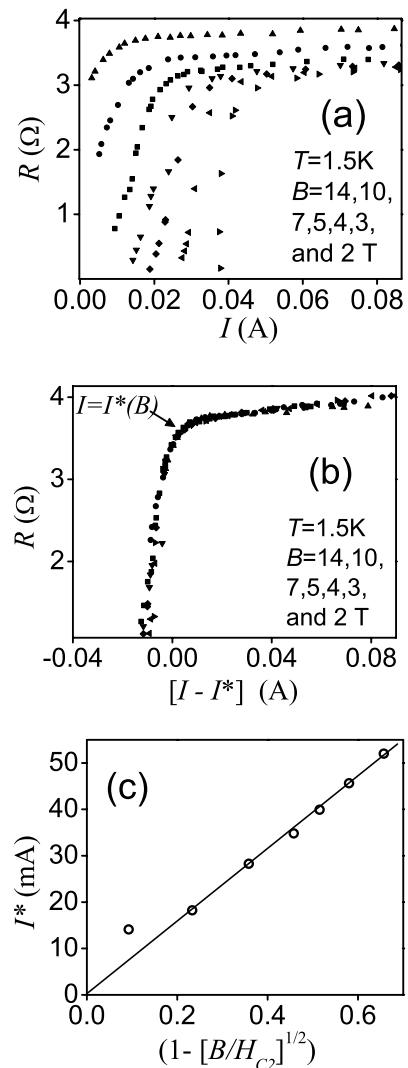


FIG. 3: (a) Resistance versus current curves for sample M. Flux densities are indicated from left to right. (b) The same data now plotted with simple vertical and horizontal shifts to produce a single collapsed curve. The horizontal shifts are by the amount I^* , the destruction current, defined at the elbow of the curve as indicated by the arrow. (c) Plot of the destruction current versus the pinch-off function $(1 - \sqrt{B/H_{c2}})$.

able cross section which is given by the factor $[1 - \sqrt{B/H_{c2}}]$. Fig. 4 shows a similar set of curves for sample S (sample L also looks similar). In all cases, the $R(I)$ curves at different flux densities collapse when shifted. And I^* , which amounts to the horizontal shift along the current axis, is proportional to the pinch-off function consistent with our simple model of vortices choking of the current-carrying cross section (other effects like pair-breaking by the field and rise in R due to vortex motion seem to be secondary).

SUMMARY

We have investigated the low-temperature ($T \ll T_c$) in-field transport behavior of MgB_2 and present the first measurement of the full dissipation curves (i.e., $0 \lesssim j \lesssim j_d$ and $0 \leq R(T=0) \lesssim R_n$) for this system. MgB_2 films made by

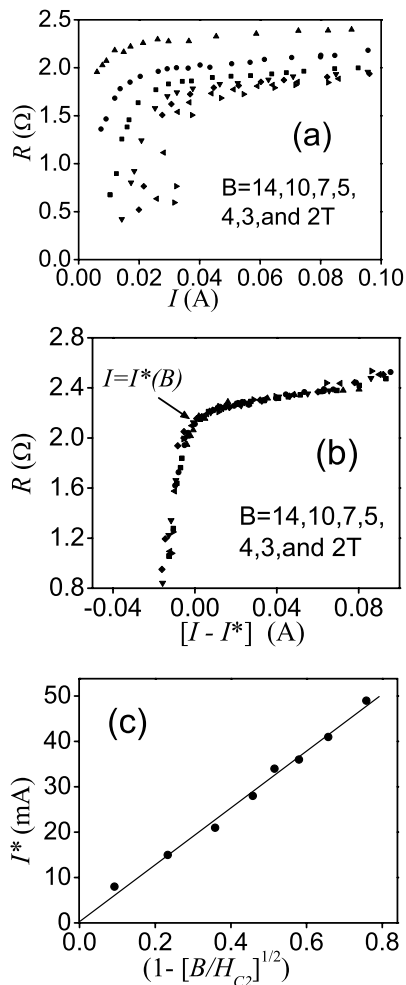


FIG. 4: Data plots for sample S. (a) Resistance versus current curves. Flux densities are indicated from left to right. (b) The collapsed data plotted after simple vertical and horizontal shifts. (c) The destruction current (defined at the elbow of the $R(I)$ curve in above panel) plotted versus the pinch-off function $[1 - \sqrt{B/H_{c2}}]$.

the two-step laser-ablation process have intrinsically strong pinning, leading to unusually steep IV and $R(I)$ curves. The onset of dissipation is within an order of magnitude of the

pairbreaking current, even at flux densities of a few Teslas, and the resistance quickly rises to the full normal-state value as the current is increased beyond j_c . The dissipation curve seems to be controlled mainly by the pair-breaking action of the current, the vortices merely serving to reduce the effective cross section over which the transport current is able to flow. Such a “pinch-off” model provides a first-order explanation of the relative horizontal (current-axis) displacements of the $R(I)$ curves at different flux densities.

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